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FRNT05 Nonlinear Control Systems and Servo Systems

Lecture 2: Linearization and Phase plane analysis

YIANNIS KARAYIANNIDIS, ASSOCIATE PROFESSOR www.yiannis.info
AUTOMATIC CONTROL, FACULTY OF ENGINEERING. yiannis@control.lth.se



Outline

- Linearization around equilibrium
- Phase plane analysis of linear systems

Material

- Glad and Ljung: Chapter 13
- Khalil: Chapter 2.1–2.3
- Lecture notes

Linearization around an equilibrium point

- Linear systems with non-zero equilibrium points

Change of variables to move the origin to the equilibrium point

Example $\dot{x} = Ax + b$ $\dot{x} \equiv 0$

$Ax + b = 0$ Equilibrium $x^* = -A^{-1}b$

A full rank New variable $\tilde{x} = x - x^*$

$x = \tilde{x} + x^*$
 $\dot{\tilde{x}} = \dot{x}$ \rightarrow constant

$\dot{\tilde{x}} = A\tilde{x}$

- Linear approximation of nonlinear systems (Taylor expansion) $f(x) = \sum_{n=0}^{\infty} \frac{f^{(n)}(a)}{n!} (x - a)^n$

$\dot{x} = f(x)$

$\dot{\tilde{x}} = \dot{x}$

$\dot{x} \equiv 0$ Equilibrium $f(x^*) = 0$

$x = \tilde{x} + x^*$

$\dot{\tilde{x}} = f(\tilde{x} + x^*)$

New variable $\tilde{x} = x - x^*$



Linearization around an equilibrium point

- Linear approximation of nonlinear systems (Taylor expansion)

$$\dot{\tilde{x}} = f(\tilde{x} + x^*) \quad \longrightarrow \quad \dot{\tilde{x}} = f(x^*) + \left. \frac{\partial f(\tilde{x} + x^*)}{\partial \tilde{x}} \right|_{\tilde{x}=0} \tilde{x} + \text{H.O.T.}$$

$$\tilde{x} = x - x^*$$

$$f(x) = f(x^*) + J_f(x^*)\tilde{x} + \frac{1}{2}\tilde{x}^T H_f(x^*)\tilde{x} + \dots$$

Jacobian **Hessian**

e.g. $f(x) = \begin{bmatrix} x_2 \\ f_2(x_1, x_2) \end{bmatrix}$

$$\dot{\tilde{x}} = f(x^*) + \frac{\partial f}{\partial x}(x^*)\tilde{x} + \text{H.O.T.}$$

Equilibrium

$$f(x^*) = 0$$

$$J_f(x) = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} & \dots & \frac{\partial f_1}{\partial x_n} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} & \dots & \frac{\partial f_2}{\partial x_n} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial f_n}{\partial x_1} & \frac{\partial f_n}{\partial x_2} & \dots & \frac{\partial f_n}{\partial x_n} \end{bmatrix}$$

$$J_f = \begin{bmatrix} 0 & 1 \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix}$$

$$\dot{\tilde{x}} \approx \frac{\partial f}{\partial x}(x^*)\tilde{x} + \text{H.O.T.}$$

$$\dot{\tilde{x}} \approx \frac{\partial f}{\partial x}(x^*)\tilde{x}$$

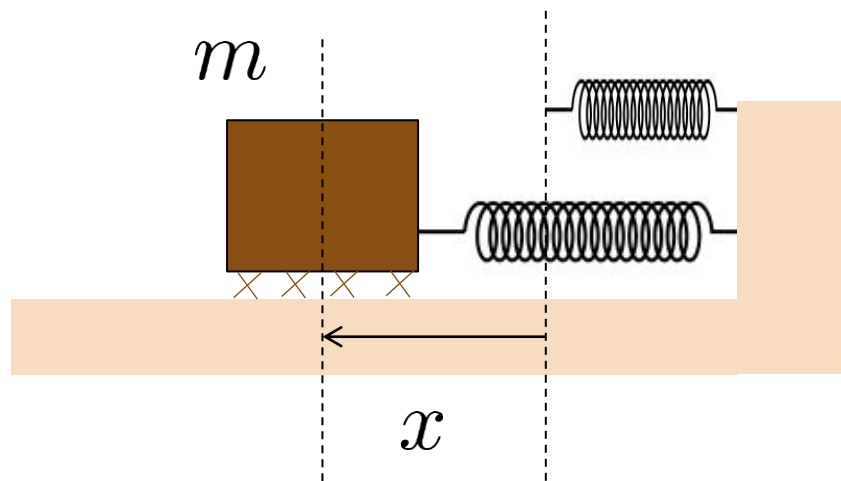
for small scalar \tilde{x}

$$f(\tilde{x}) \approx 2\tilde{x} + \tilde{x}^2$$

$$\Rightarrow \tilde{x}^2 \ll \tilde{x}$$

$$f(\tilde{x}) \approx 2\tilde{x}$$

Example (nonlinear spring with external force)



- Differential Equation

$$m\ddot{x} + k_v\dot{x} + k_s x^3 = F$$

- State space representation

Position: $\underline{x_1 = x}$ Velocity: $\underline{x_2 = \dot{x}}$

$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -\frac{k_s}{m}x_1^3 - \frac{k_v}{m}x_2 + \frac{F}{m}$$

- State space representation (vector form) $\underline{x} = \begin{bmatrix} x_1 & x_2 \end{bmatrix}^T$

$$\underline{\dot{x}} = \underline{f(x)} \quad \begin{bmatrix} f_1(x) \\ f_2(x) \end{bmatrix} \underline{f(x)} = \begin{bmatrix} x_2 \\ -\frac{k_s}{m}x_1^3 - \frac{k_v}{m}x_2 + \frac{F}{m} \end{bmatrix}$$

$$\dot{x}_1 = f_1(x) = x_2$$

$$\dot{x}_2 = f_2(x) = -\frac{k_s x_1^3}{m} - \frac{k_v x_2}{m} + \frac{F}{m}$$

$$\text{Equilibrium} \left\{ \begin{array}{l} x_2 = 0 \\ \dot{x}_1 = 0 \\ \dot{x}_2 = 0 \end{array} \right.$$

$$k_s x_1^3 = F \Rightarrow x_1^3 = \frac{F}{k_s} \Rightarrow x_1 = \left(\frac{F}{k_s}\right)^{1/3}$$

Jacobian

$$J_f = \frac{\partial f}{\partial x} = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{3k_s x_1^2}{m} & -\frac{k_v}{m} \end{bmatrix}$$

$$J_f(x^*) = J_f \left(\underbrace{\left(\frac{F}{k_s}\right)^{1/3}}_{x_{1,eq}}, \underbrace{0}_{x_{2,eq}} \right)$$

Jacobian calculated at equil.

$$J_f(x^*) = \frac{\partial f}{\partial x}(x^*) =$$

$$\begin{bmatrix} 0 & 1 \\ -\frac{3k_s}{m} \left(\frac{F}{k_s}\right)^{2/3} & -\frac{k_v}{m} \end{bmatrix}$$

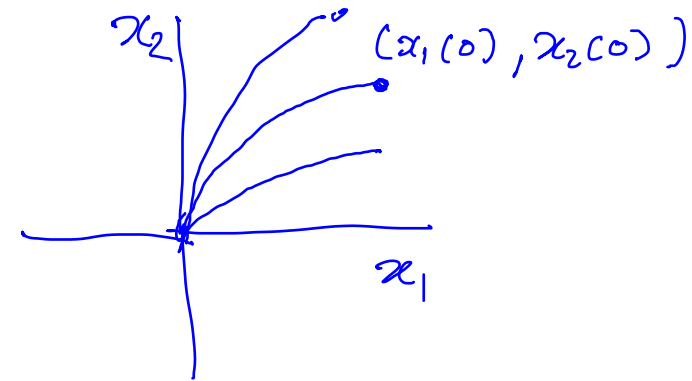


Phase plane analysis

- The phase plane method is the graphical study of second-order autonomous systems:

$$\dot{x}_1 = f_1(x_1, x_2)$$

$$\dot{x}_2 = f_2(x_1, x_2)$$

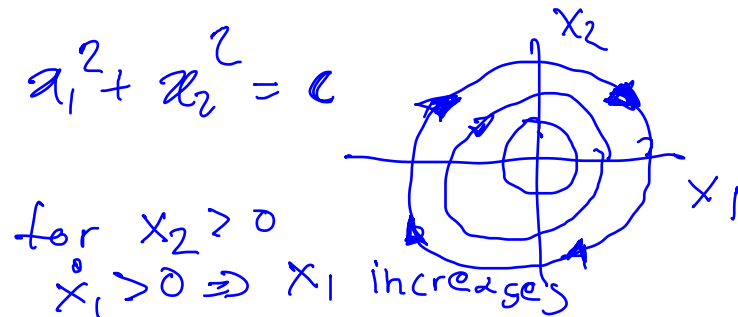


- Phase plane has x_1 and x_2 as coordinates.
 $\Rightarrow x_1(t)$
 $x_2(t)$
- Phase plane trajectory: a curve of the phase plane representing the solution for initial conditions $x_1(0), x_2(0)$ with time t varied from 0 to infinity
- Phase portrait: a family of phase plane trajectories from various initial conditions

- Example: $\ddot{y} + y = 0$ $x_1 = y(t) = \mathcal{C} \sin(t + \phi_0)$

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= -x_1 \end{aligned}$$

$$x_2 = \dot{y}(t) = \mathcal{C} \cos(t + \phi_0)$$



A first glimpse on phase portraits

$$\dot{x}_1 = f_1(x_1, x_2) = x_1^2 + x_2$$

$$\dot{x}_2 = f_2(x_1, x_2) = -x_1 - x_2$$

Eq $x_1^2 + x_2 = 0 \Rightarrow x_1^2 - x_1 = 0$
 $-(x_1 + x_2) = 0 \Rightarrow x_2 = -x_1$ (*)

$x_1 = 0 \quad x_1 = 1$
 $x_2 = 0 \quad x_2 = -1$

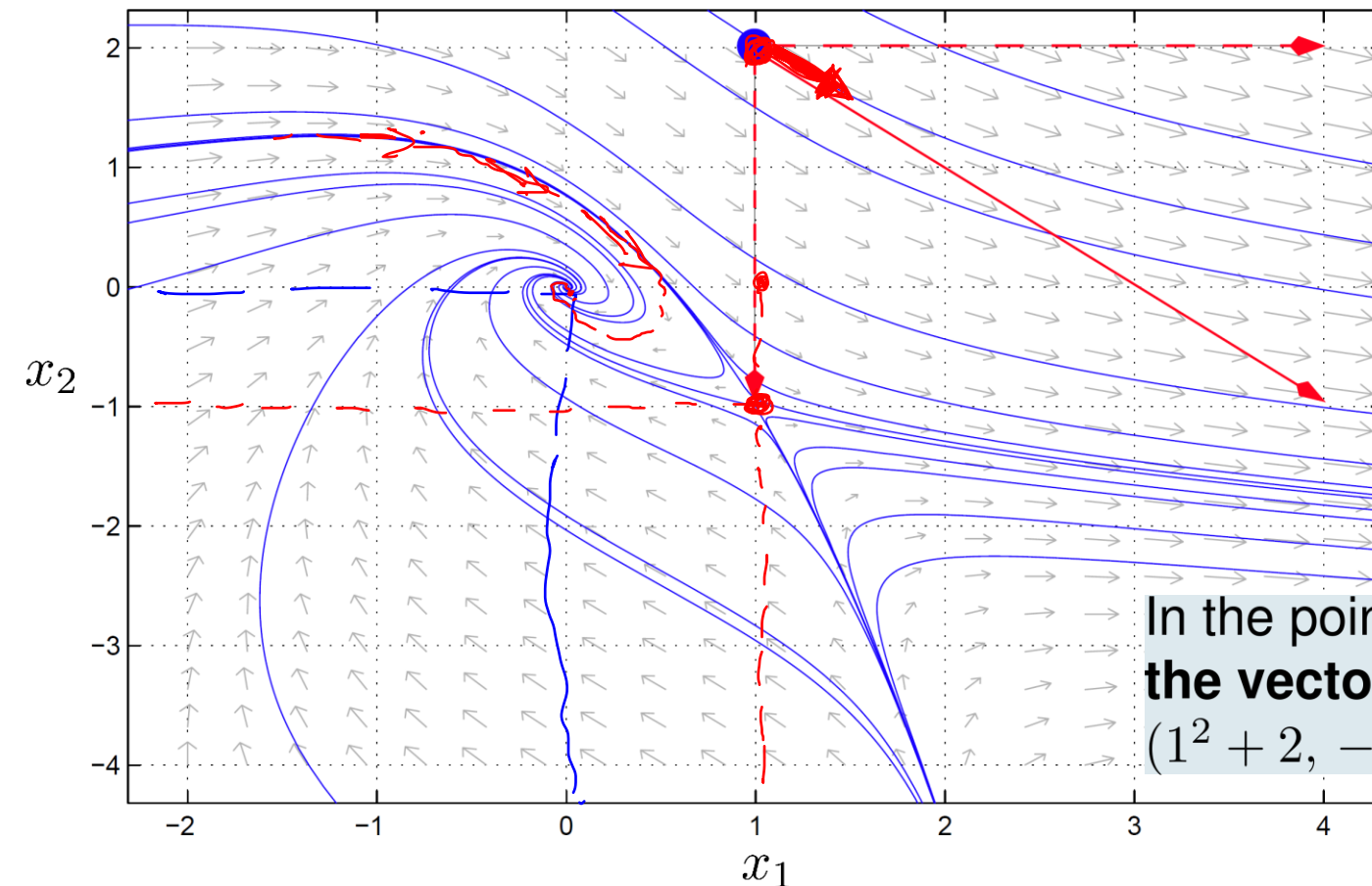
• The **vector field** $f(x_1, x_2) = \begin{bmatrix} f_1(x_1, x_2) \\ f_2(x_1, x_2) \end{bmatrix}$

is tangent at point (x_1, x_2) because

$$\frac{dx_2}{dx_1} = \frac{f_1(x_1, x_2)}{f_2(x_1, x_2)}$$

- The slope is indeterminate at equilibrium points aka singular points
- Don't forget the arrows!

In the point $(x_1, x_2) = (1, 2)$
 the **vector field** is pointing in the direction
 $(1^2 + 2, -1 - 2) = (3, -3)$.



Solution of Linear Systems of diff. eq.

State space representation: $\dot{x} = \boxed{Ax}$

$$\dot{x} = \alpha x \Rightarrow x(t) = x(0) e^{\alpha t}$$

Similar to scalar

Solution: $\dot{x} = e^{\boxed{At}} x(0)$

$$z = Wx$$

Similarity transformation and change of variables:

$$\dot{x} = \boxed{Ax} \Rightarrow \dot{x} = W^{-1} M W x \Rightarrow \boxed{\dot{z} = Mz}$$

Real distinct eigenvalues λ_1, λ_2

One double eigenvalue λ

Complex Eigenvalues $\sigma \pm j\omega$

$$M = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}$$

$$M = \begin{bmatrix} \lambda & 1 \\ 0 & \lambda \end{bmatrix}$$

$$M = \begin{bmatrix} \sigma & -\omega \\ \omega & \sigma \end{bmatrix}$$

Two real eigenvectors

Complex eigenvectors

$$W = \begin{bmatrix} v_1 & v_2 \end{bmatrix}$$

Eigenvalues
 $\det(\lambda I - A) = 0$

$$W = \begin{bmatrix} v & R_{\frac{\pi}{2}} v \end{bmatrix}$$

Eigenvectors
 $Av = \lambda v$

$$W = \begin{bmatrix} \overset{\text{Real}}{\Re(v_1)} & \Im(v_1) \end{bmatrix}$$

$$R = \begin{bmatrix} \cos \frac{\pi}{2} & \sin \frac{\pi}{2} \\ -\sin \frac{\pi}{2} & \cos \frac{\pi}{2} \end{bmatrix}$$

Rotation matrix

Imaginary

Solution of Linear Systems of diff. eq.

State space representation after change of variables $z = W^{-1}x$: $\dot{z} = Mz$

Solution for the new state: $z(t) = e^{Mt}z(0)$

Real distinct eigenvalues $e^{Mt} = \text{diag}(e^{\lambda_1 t}, e^{\lambda_2 t})$

$$W = \begin{bmatrix} v_1 & v_2 \end{bmatrix}$$

One double eigenvalue $e^{Mt} = \text{diag}(e^{\lambda t} + te^{\lambda t}, e^{\lambda t})$

$$W = \begin{bmatrix} v & R_{\frac{\pi}{2}}v \end{bmatrix}$$

Complex Eigenvalues $e^{Mt} = e^{\sigma t} e^{\omega t S} = e^{\sigma t} \underbrace{R_{\omega t}}_{\begin{bmatrix} \cos(\omega t) & \sin(\omega t) \\ -\sin(\omega t) & \cos(\omega t) \end{bmatrix}}$

$$W = \begin{bmatrix} \Re(v_1) & -\Im(v_1) \end{bmatrix}$$

Solution of the original state: $x(t) = W^{-1}z(t) = W^{-1}e^{Mt}z(0)$

Two real eigenvalues

Direct elimination of time variable

$$\begin{aligned} \dot{x}_1 &= \lambda_1 x_1 \\ \dot{x}_2 &= \lambda_2 x_2 \end{aligned}$$



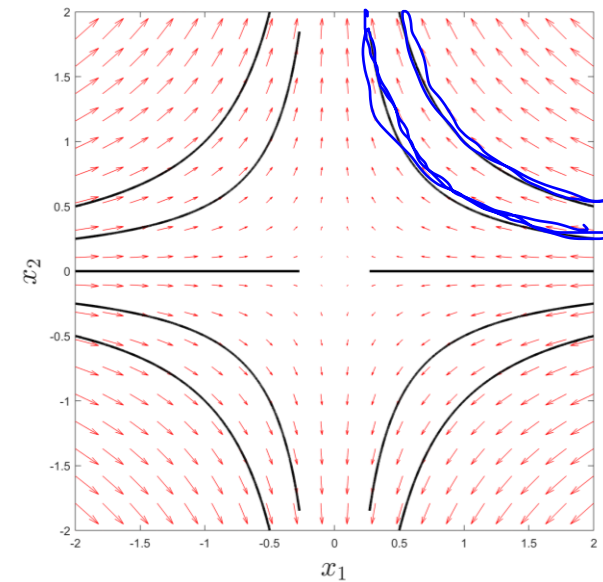
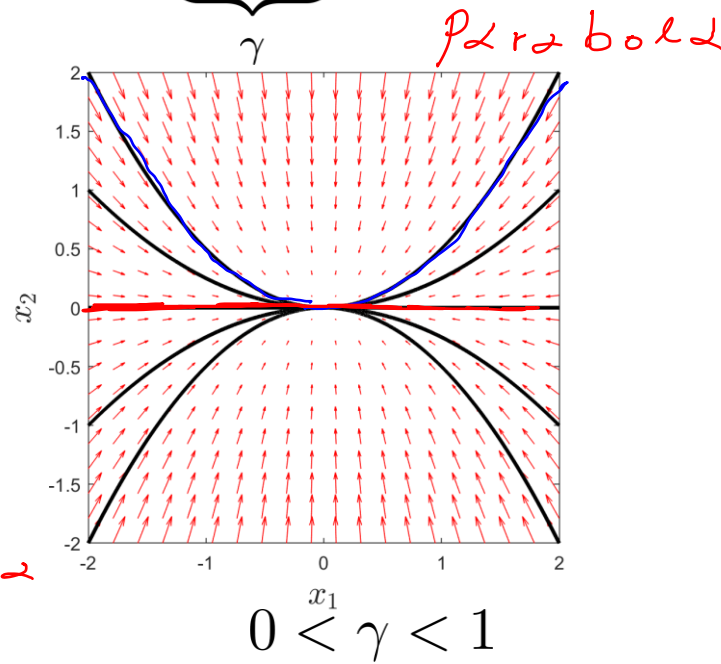
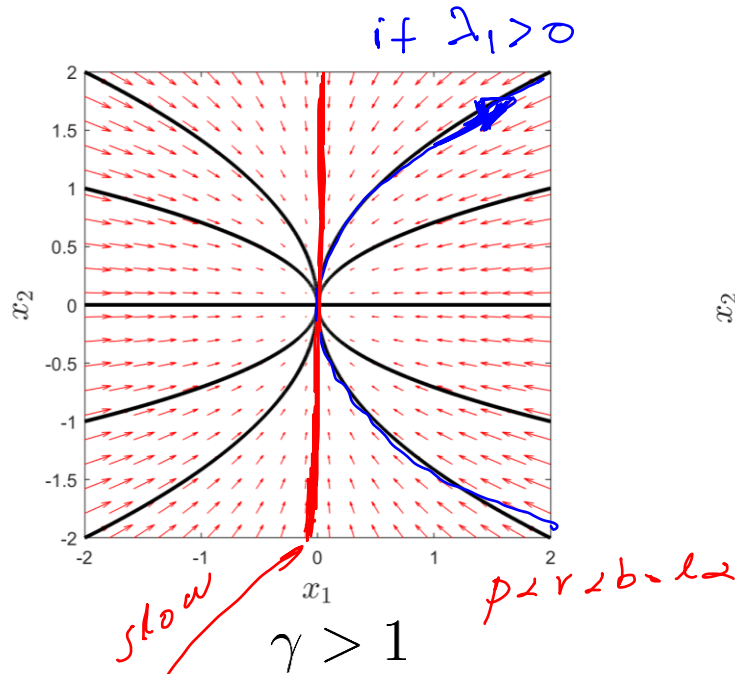
$$\frac{dx_1}{dx_2} = \underbrace{\left(\frac{\lambda_1}{\lambda_2} \right)}_{\gamma} \frac{x_1}{x_2}$$



$$\frac{dx_1}{x_1} = \gamma \frac{dx_2}{x_2}$$



$$x_1 = C x_2^\gamma$$



Hyperbola

$$\gamma < 0$$

$$\lambda_2 < 0 < \lambda_1$$

$$\underbrace{\lambda_1}_{\text{faster}} < \underbrace{\lambda_2}_{\text{slower}} < 0 \quad 0 < \underbrace{\lambda_2}_{\text{slower}} < \underbrace{\lambda_1}_{\text{faster}}$$

$$\begin{aligned} x_1 &= C x_2^\gamma \\ \Rightarrow x_2 &= \left(\frac{1}{C} x_1 \right)^{1/\gamma} \end{aligned}$$

Two real eigenvalues

$$\underbrace{\lambda_1}_{\text{faster}} < \underbrace{\lambda_2}_{\text{slower}} < 0$$

$v_1 \qquad v_2$

$$x(t) = c_1 e^{\lambda_1 t} v_1 + c_2 e^{\lambda_2 t} v_2$$

Fast eigenvector

$$x(t) \approx c_1 e^{\lambda_1 t} v_1 + c_2 v_2 \quad \text{for small } t$$

Slow eigenvector

$$x(t) \approx c_2 e^{\lambda_2 t} v_2 \quad \text{for large } t$$

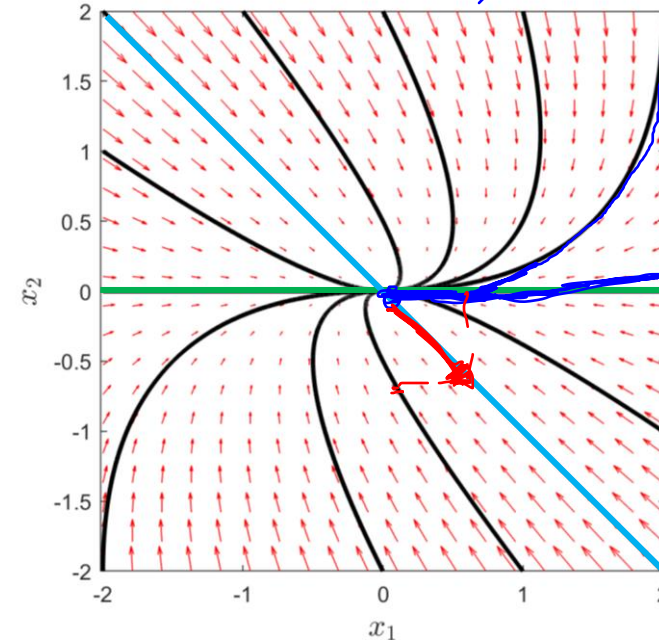
Example:

$$\dot{x} = \begin{bmatrix} -1 & 1 \\ 0 & -2 \end{bmatrix} x$$

$$[X \ Y] = \text{eigs}(A)$$

$$(\lambda_1, \lambda_2) = (-1, -2)$$

$$v_2 = \frac{\sqrt{2}}{2} [1 \ -1]^T$$

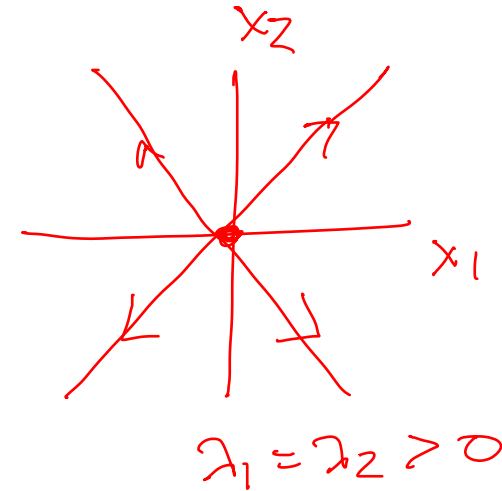
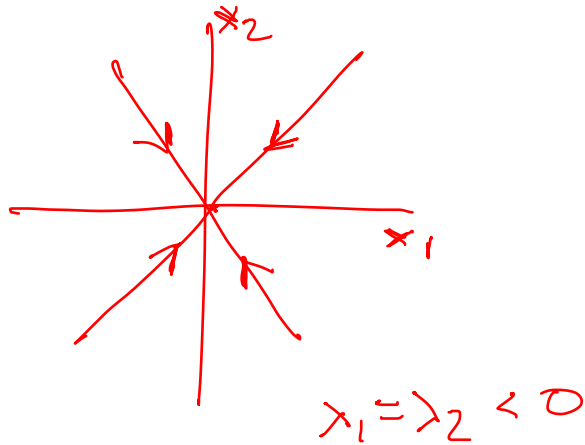


$$v_1 = [1 \ 0]^T \quad \text{slower}$$

Some comments

- What if $\lambda_1 = \lambda_2$?

$$x_1 = c x_2$$



Star

- $\lambda_1 \lambda_2 = \det(A)$

$$\lambda_1 + \lambda_2 = \text{Tr}(A)$$

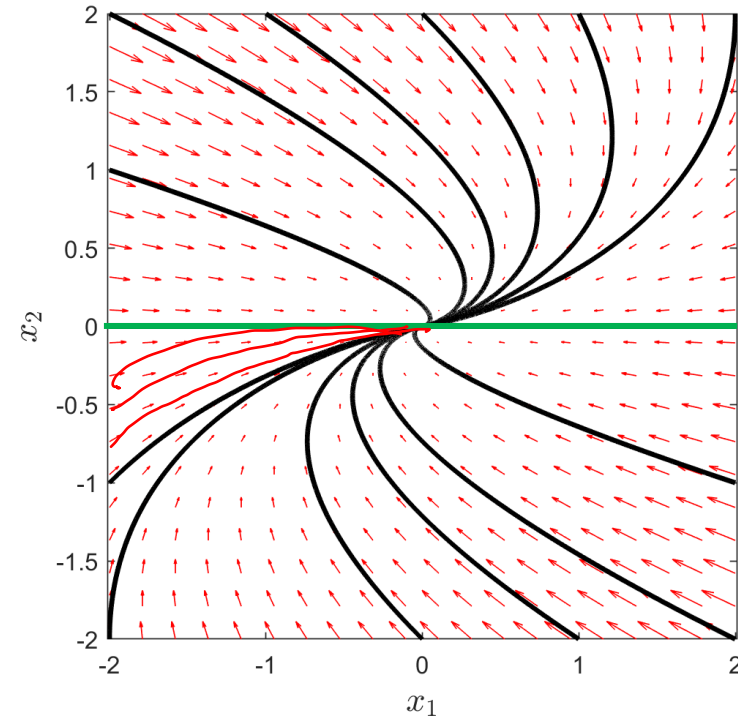
$$\lambda_{1,2} = \frac{1}{2} \left[\text{Tr}(A) \pm \sqrt{\text{Tr}^2(A) - 4\det(A)} \right]$$

One tangent mode

$$\dot{x} = \begin{bmatrix} \lambda & 1 \\ 0 & \lambda \end{bmatrix} x, \quad \text{rank}(\lambda I - A) = 1$$

$$x_1(t) = x_1(0)e^{\lambda t} + tx_2(0)e^{\lambda t}$$

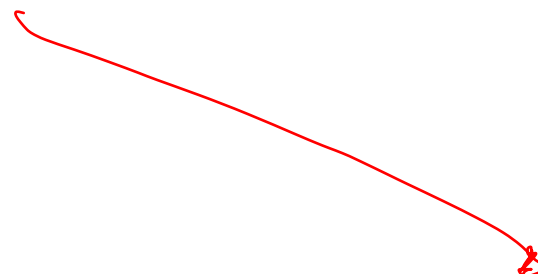
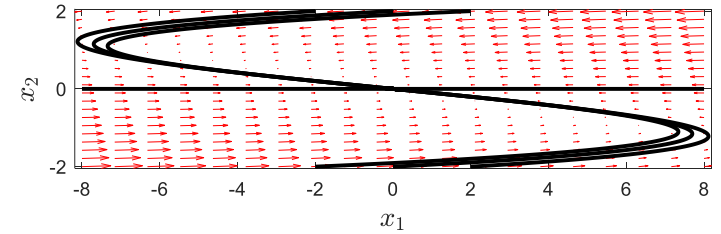
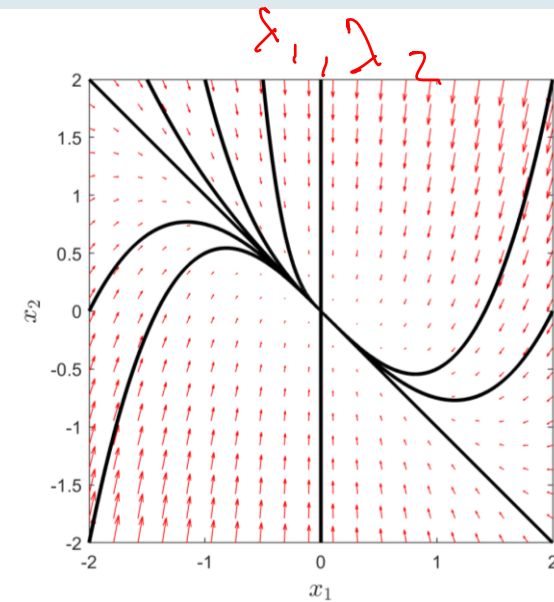
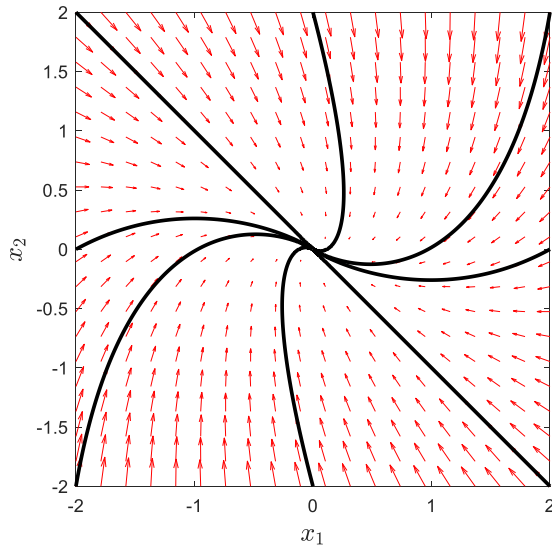
$$x_2(t) = x_2(0)e^{\lambda t}$$



$$v_1 = \begin{bmatrix} 1 & 0 \end{bmatrix}^T$$



Matching quiz 1



$$\dot{x} = \begin{bmatrix} -0.5 & 0.5 \\ -0.5 & -1.5 \end{bmatrix} x$$

$$\dot{x} = \begin{bmatrix} -1 & -10 \\ 0 & -1 \end{bmatrix} x$$

$$\dot{x}_2 = -x_2$$

$$\dot{x} = \begin{bmatrix} -1 & 0 \\ -2 & -3 \end{bmatrix} x$$

Complex eigenvalues

$$\dot{x} = Ax \quad \xrightarrow{z = W^{-1}x} \quad \dot{z} = \begin{bmatrix} \sigma & -\omega \\ \omega & \sigma \end{bmatrix} z$$

$\sigma \pm j\omega$

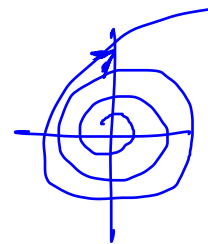
$$W = \begin{bmatrix} \Re(v_1) & \Im(v_1) \end{bmatrix}$$

$$r = \sqrt{z_1^2 + z_2^2}, \quad \theta = \arctan z_2/z_1$$

$$z_1 = r \cos \theta, \quad z_2 = r \sin \theta$$

$$\begin{aligned} \dot{r} &= \sigma r \\ \dot{\theta} &= \omega \end{aligned}$$

Why?

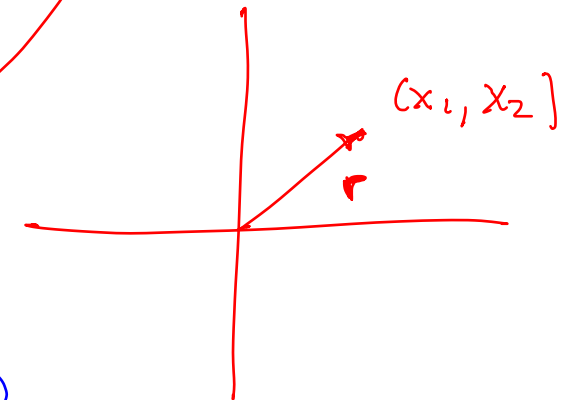
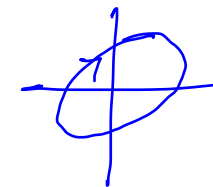


$$\dot{r} = 6r$$

$$\dot{r} = 0$$

$$\dot{r} = -2r$$

$$r \rightarrow 0$$



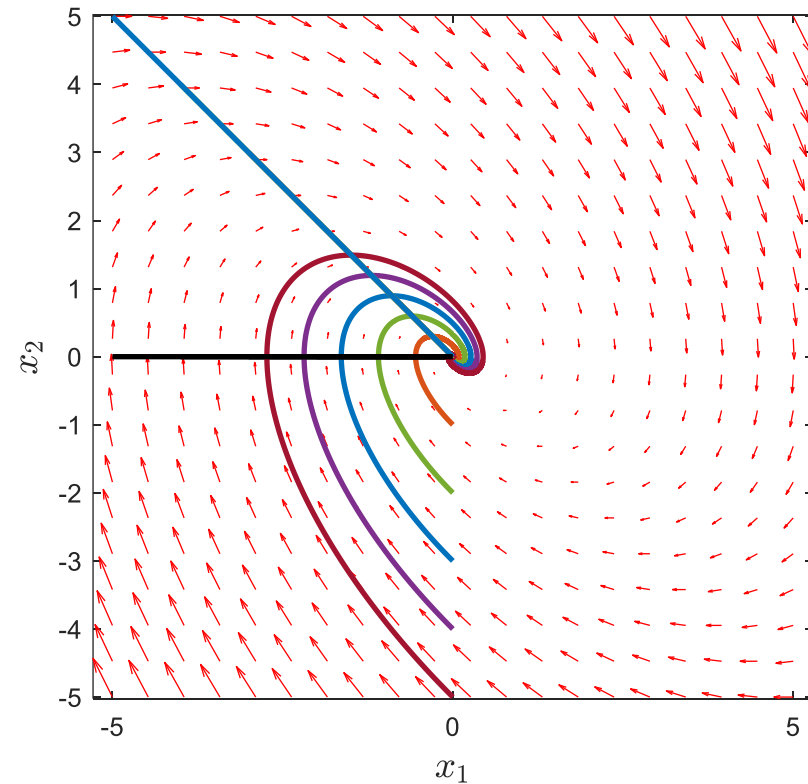
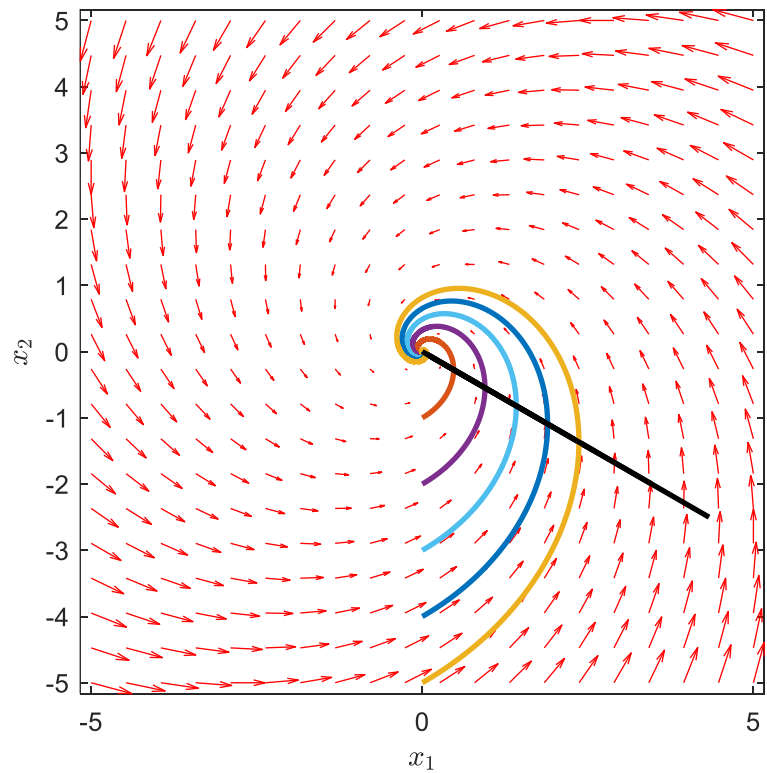
If $\sigma > 0$ Unstable focus

If $\sigma = 0$ Center

If $\sigma < 0$ Stable focus

Matching quiz 2

$$\dot{x} = \frac{1}{2} \begin{bmatrix} -1 & -\sqrt{3} \\ \sqrt{3} & -1 \end{bmatrix} x \quad \lambda_{1,2} = -\frac{1}{2} \pm \frac{\sqrt{3}}{2}j \quad \dot{x} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} x$$

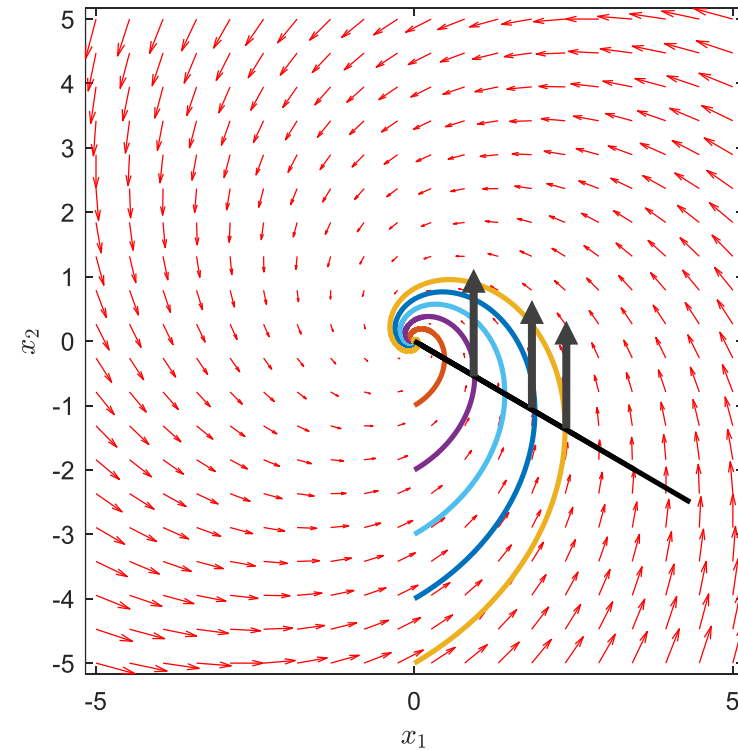
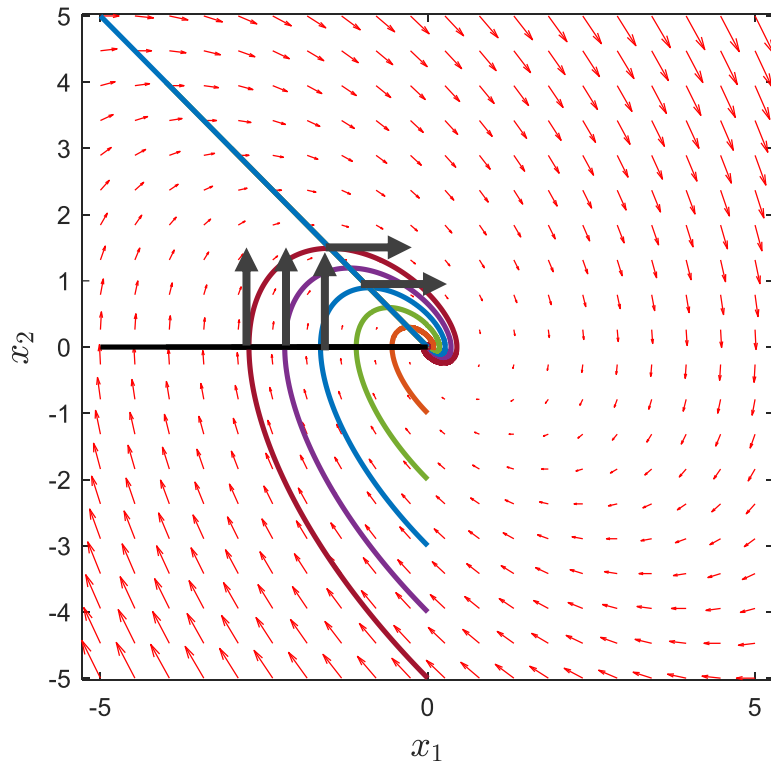


Example

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} x \quad \longrightarrow \quad \lambda_{1,2} = -\frac{1}{2} \pm \frac{\sqrt{3}}{2}j$$

$$\dot{z} = \frac{1}{2} \begin{bmatrix} -1 & -\sqrt{3} \\ \sqrt{3} & -1 \end{bmatrix} z \quad \longrightarrow \quad \begin{aligned} \dot{r} &= -\frac{1}{2}r \\ \dot{\theta} &= \frac{\sqrt{3}}{2} \end{aligned}$$

- Stable focus $\sigma = -1/2 < 0$



How to draw phase portraits

If done by hand then

1. Find equilibria (also called singularities)
2. Sketch local behavior around equilibria
3. Sketch (\dot{x}_1, \dot{x}_2) for some other points. Use that $\frac{dx_1}{dx_2} = \frac{\dot{x}_1}{\dot{x}_2}$.
4. Try to find possible limit cycles
5. Guess solutions

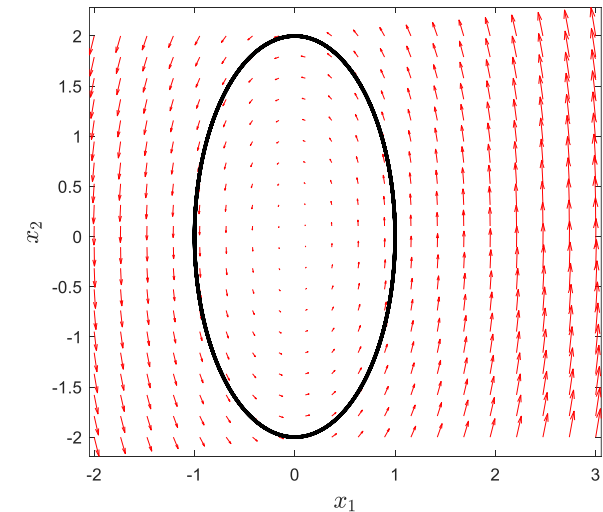
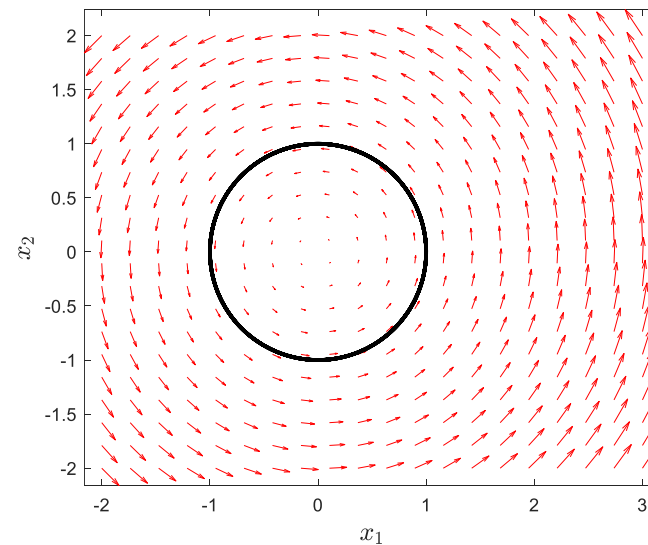
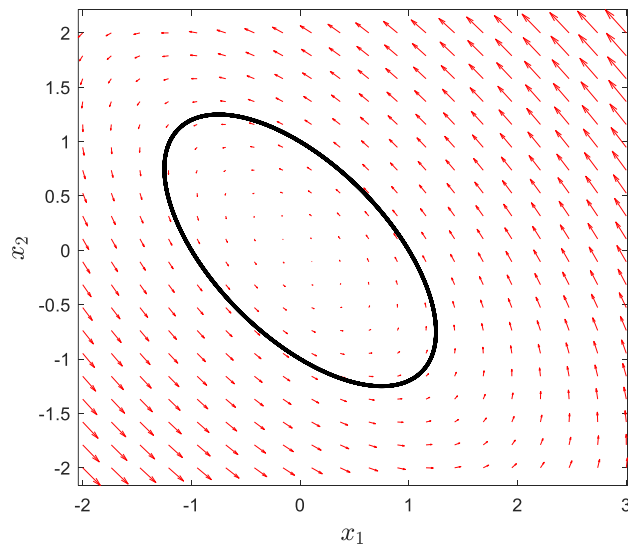
Matlab: PPTool and some other tools for Matlab is available on Canvas.

Matching quiz 3

$$\dot{x} = \begin{bmatrix} 0 & -1 \\ 4 & 0 \end{bmatrix} x$$

$$\dot{x} = \begin{bmatrix} -1.5 & -2.5 \\ 2.5 & 1.5 \end{bmatrix} x$$

$$\dot{x} = \begin{bmatrix} 0 & -2 \\ 2 & 0 \end{bmatrix} x$$



Summary of phase portraits and their equilibria

$\text{Im}\lambda_i = 0$: stable node
 $\lambda_1, \lambda_2 < 0$

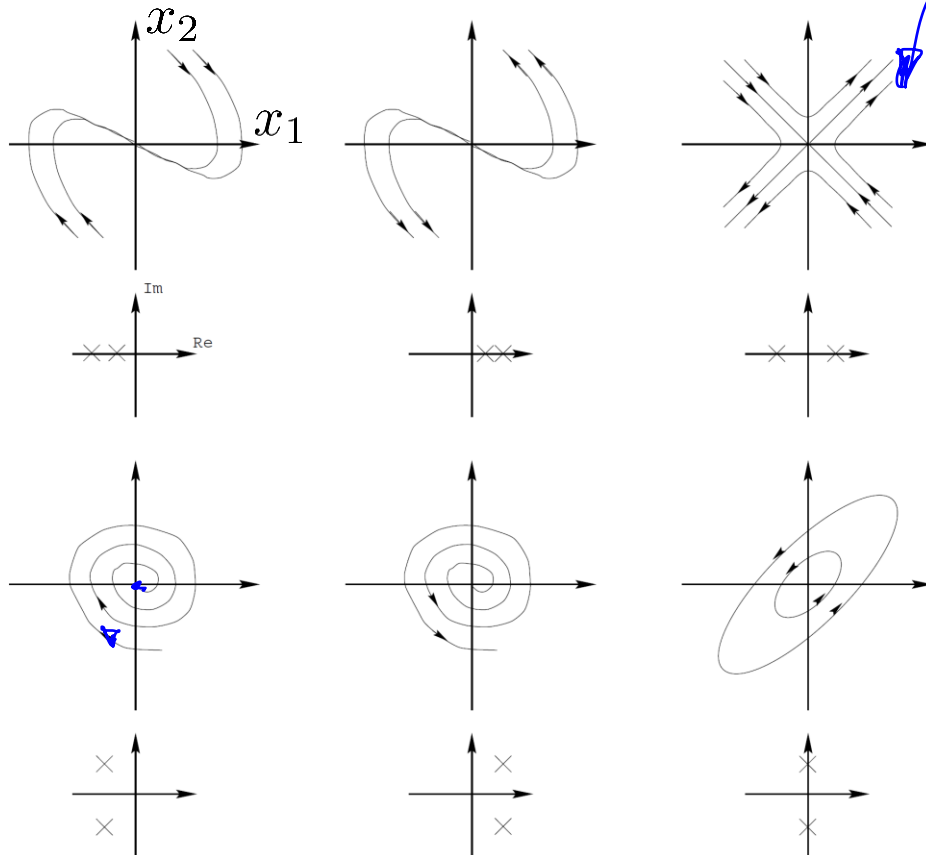
$\text{Im}\lambda_i \neq 0$: 6 $\text{Re}\lambda_i < 0$
 stable focus

unstable node
 $\lambda_1, \lambda_2 > 0$

$\text{Re}\lambda_i > 0$
 unstable focus

saddle point
 $\lambda_1 < 0 < \lambda_2$

$\text{Re}\lambda_i = 0$
 center point



Effect of perturbations

Perturbations in $A + \Delta$

- Structurally stable: the qualitative behavior remains the same under arbitrarily small perturbations in A

Examples: a node (with distinct eigenvalues), a saddle or a focus

- A stable node with multiple eigenvalues could become a stable node or a stable focus under arbitrarily small perturbations in A
- A center is not structurally stable

$$\dot{z} = \begin{bmatrix} 0 & -\omega \\ \omega & 0 \end{bmatrix} z \quad \longrightarrow \quad \dot{z} = \begin{bmatrix} \delta & -\omega \\ \omega & \delta \end{bmatrix} z \quad \delta \pm j\omega$$

Back to linearization

Theorem Assume

$$\dot{x} = f(x)$$

is linearized at x^* so that

$$\dot{\tilde{x}} = A\tilde{x} + g(x),$$

where

- $A = \frac{\partial f}{\partial x}(x^*)$
- $g = f(x) - \frac{\partial f}{\partial x}(x^*)\tilde{x} \in C^1$ and $\frac{\|g(x)\|}{\|\tilde{x}\|} \rightarrow 0$ as $\|\tilde{x}\| \rightarrow 0$

If $\dot{\tilde{x}} = A\tilde{x}$ has a focus, node, or saddle point, then $\dot{x} = f(x)$ has the same type of equilibrium at the origin.

If the linearized system has a center, then the nonlinear system has either a center or a focus.

Back to linearization

Summary

- Linearization

$$\dot{x} = f(x) \Rightarrow \dot{\tilde{x}} = A\tilde{x} + g(x),$$

- Phase portraits of Linear systems
- Whether the behavior of the Linear system (outcome of linearization) can be inherited to the nonlinear system?